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Synthesis and magnetic properties of ZnFe₂O₄ obtained by mechanochemically assisted low-temperature annealing of mixtures of Zn and Fe oxalates

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Abstract

The mechanism of formation of zinc ferrite $(ZnFe_2O_4)$ from $ZnC_2O_4 \cdot 1.8H_2O - 2Fe^{II}C_2O_4 \cdot 2H_2O$ and $ZnC_2O_4 \cdot 1.8H_2O - Fe_2^{III}(C_2O_4)_3 \cdot 6H_2O$ mixtures is investigated. By combination of TG and XRPD measurements it has been shown that microcrystalline $ZnFe_2O_4$ forms from physical mixtures after prolonged annealing at 1000 °C while nanocrystalline $ZnFe_2O_4$ powders are produced by mild annealing (1 h at 500 °C in air) of mechanically activated mixtures. The magnetic properties of $ZnFe_2O_4$ powders obtained from physical and from milled mixtures are compared. © 2006 Elsevier B.V. All rights reserved.

Keywords: Zinc ferrite; Mechanical activation; Magnetic properties

1. Introduction

Ferrites are technologically important ceramic materials that have been studied and utilized for many years. Recently, the nanotechnology has spurred renewed interest in these materials. ZnFe₂O₄ crystallizes with a spinel lattice with Zn²⁺ in tetrahedral interstices and Fe³⁺ in the octahedral ones (direct spinel structure). Actually in nanosized ferrites it was observed that the distribution of cations in octahedral and tetrahedral sites changes as the crystallite size decreases [1] and that this fact leads to the unusual phenomenon of superparamagnetism on heating. Several synthetic routes to prepare nanosized ZnFe₂O₄ have been proposed. Besides the classical methods of coprecipitation [2], hydrothermal synthesis [3] and sol-gel [4], suitably modified methods have been proposed such as a synthetic route that, starting from metallic chloride solutions and using aqueous ammonia at pH 9 (180 °C), leads to 4 nm—ZnFe₂O₄ powders with magnetic susceptibility about two orders of magnitude higher than that of typical paramagnetic substances [5]. Furthermore, a modified coprecipitation synthesis process has been

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realized by heating under nitrogen a solution of Fe(II) sulphate and Zn(II) acetate with urea [6]. Again a wet synthesis starting from a solution of zinc chloride and iron(II) chloride [7] and a low temperature synthesis by using hydrazine monohydrate [8] have been performed. Finally direct mechanochemical synthesis has been realized starting from the constituent oxides $(ZnO + Fe_2O_3)$ [9].

In the present work, we report a synthesis of nanometric $ZnFe_2O_4$ from a combination of mechanical activation of solid mixtures of metal oxalates $[ZnC_2O_4 \cdot 1.8H_2O + 2FeC_2O_4 \cdot 2H_2O$ or $ZnC_2O_4 \cdot 1.8H_2O + Fe_2(C_2O_4)_3 \cdot 6H_2O]$ followed by mild annealing (1 h at 500 °C) under air flow. A study of the reaction mechanism has been performed by TG/DSC. Moreover, the dependence of the magnetic properties on the mechanical treatment is reported.

2. Experimental

2.1. Starting chemicals and samples preparation

The starting chemicals have been purchased by Aldrich Chimica (Italy): $ZnC_2O_4 \cdot 2H_2O$ (purity 99.9%), $FeC_2O_4 \cdot 2H_2O$ (purity 99.9%) and $Fe_2(C_2O_4)_3 \cdot 6H_2O$ (purity 99.9%). The

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hydration extent of the starting chemicals has been assessed by TG measurements: the number of water molecules of the two iron oxalates has been confirmed to coincide with the nominal one while that of the Zn compound resulted slightly less (1.81 versus 2). Physical mixtures (PM) of molar ratio Zn:Fe 1:2 have been prepared by weighing the appropriate amounts of the two components and by stirring them in acetone suspension for 3 h. Then the solvent has been evaporated in oven at 60 °C overnight. The mechanically activated mixtures (MM) have been prepared by dry milling lots of 2 g of the PM. The powders have been put into agate jars (12.5 mL) of a planetary mill (Pulverisette 7 by Fritsch, Germany) with three agate balls (12 mm diameter; ball/sample mass ratio 3:1). The mill has been operated at 500 rpm rotation speed for 50 h (1 h milling, 0.5 h pause). No addition of silica has been recorded by XRPD after the milling.

2.2. Experimental techniques

- TGA measurements have been performed by a 2950 thermogravimetric analyser (TA Instruments Inc., USA) connected to a TA 5000 computer (also by TA Instruments Inc., USA). Both PM and MM samples (about 50 mg) have been placed in a Pt-Rh pan and heated at 5 K/min (under air flow of 100 mL/min) from 25 °C up to 500 °C.
- Simultaneous DSC/TGA measurements have been performed with a STA 625 by Polymer Laboratories (UK) connected to a data station with proprietary software. Samples (≈10 mg) of MM have been placed in an aluminium pan and heated (under air flow of 120 mL/min) at 5 K/min from 25 °C up to 500 °C. The enthalpy values have been determined from the

area of the DSC peaks recorded after calibration has been performed using sapphire (for heat capacity calibration) and indium–zinc (both for enthalpy and temperature calibration).

- X-ray powder diffraction patterns have been recorded in step scan mode (step 0.015°, 1 s/step, 40 kV, 30 mA) by a X-ray powder diffractometer (Bruker D5005) equipped with a Position Sensitive Detector (PSD, Braun). XRPD patterns have been recorded on the following samples: (i) samples of PM and MM recovered after the thermoanalytical scans in order to identify the compounds formed during thermal treatment; (ii) samples of both PM and MM heated (5 K/min under air flow) up to 500 °C and annealed for 1 h. The crystal size of ZnFe₂O₄ powders prepared from MM under air flow has been calculated by the Scherrer equation. The instrumental line broadening has been determined from the patterns of a ZnFe₂O₄ sample prepared from a physical mixture ZnO–Fe₂O₃ annealed 36 h at 1000 °C.
- Samples of both physical and milled mixtures have been examined by scanning electron microscopy (SEM, Model Stereoscan 200 by Cambridge, UK). Samples of ZnFe₂O₄ prepared by annealing MM have also been observed with SEM electron microscope. Before analysis all the samples have been sputtered under vacuum with gold metal.
- Specific surface area of both PM and MM has been determined by the BET method (N₂ adsorption, Sorptomatic 1990, Thermo Electron Corporation).
- Magnetic properties have been measured in a Quantum Design SQUID magnetometer. The magnetic moment as a function of temperature was measured in a magnetic field of 100 Oe. Hysteresis loop at different temperatures were measured in magnetic field up to 5 T.



Fig. 1. SEM micrographs of (a) $ZnC_2O_4 \cdot 1.8H_2O - 2FeC_2O_4 \cdot 2H_2O$ physical mixture; (b) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ physical mixture; (c) $ZnC_2O_4 \cdot 1.8H_2O - 2FeC_2O_4 \cdot 2H_2O$ milled mixture; (d) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ milled mixture; (d) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ milled mixture; (d) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ milled mixture; (d) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ milled mixture; (d) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ milled mixture; (d) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ milled mixture; (d) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ milled mixture; (d) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ milled mixture; (d) $ZnC_2O_4 \cdot 1.8H_2O - Fe_2(C_2O_4)_3 \cdot 6H_2O$ milled mixture.



Fig. 2. TG (solid line) and DTG (dashed line) curves of $ZnC_2O_4 \cdot 1.8H_2O-2FeC_2O_4 \cdot 2H_2O$ physical mixture heated at 5 K/min up to 500 °C under air flow.

3. Results and discussion

Fig. 1 reports the micrographs of samples of both physical (Fig. 1a and b) and milled (Fig. 1c and d) mixtures. The physical mixtures show differences in the crystal morphology depending on whether Fe(II) or Fe(III) oxalate is present. This should be the consequence of the fact that ferric oxalate was more agglomerated than the ferrous one. Another difference between the two types of mixtures is revealed by the fact that the specific surface area of the Fe(II) mixture $(5.9 \text{ m}^2/\text{g})$ is three times larger that that of the Fe(III) mixture $(1.9 \text{ m}^2/\text{g})$. The specific surface area of both mixtures increases by milling but the milling effect on the surface area is more evident on the Fe(III) mixture: the surface area of the Fe(II)-based mixture rises to 9.4 m^2/g (it increases by 1.5 times), whereas that of the Fe(III)-based mixture becomes $5.2 \text{ m}^2/\text{g}$ (it increases almost three times). The higher effect of milling on the Fe(III) mixture is also evident when comparing the XRPD powder patterns of the milled mixtures. Some peaks, due to both oxalates, are indeed present in the Fe(II) mixture while complete amorphization has occurred in the Fe(III) mixture. A definite evidence of the fact that no oxalate decomposition has taken place during milling is obtained by a TG/DSC study of the processes occurring by heating the milled mixtures. Such study contributes to the understanding of the mechanism of the reaction.

3.1. Thermoanalytical measurements

3.1.1. $ZnC_2O_4 \cdot 1.8H_2O - 2FeC_2O_4 \cdot 2H_2O$ mixtures

Fig. 2 shows a typical TG/DTG curve of a PM. The first step of mass loss (ending at \approx 150 °C) is due to the dehydration of zinc oxalate. The second step ends at \approx 300 °C and corresponds to a mass of 56.27 ± 0.44% (the standard deviation represents that of five independent measurements). During this step both Fe(II) oxalate dehydration and decomposition (with partial oxidation) occur. The mass value well agrees with that expected for the formation of a mixture ZnC₂O₄-(2/3)Fe₃O₄ (56.40%). The following step of mass loss (-12.19 ± 0.53%) is lower than that expected (-13.24%) for the decomposition of ZnC₂O₄ and this is due to the oxidation of Fe₃O₄ to Fe₂O₃ that takes place during the decomposition of ZnC₂O₄. Indeed the mean final mass



Fig. 3. TG (solid line), DTG (dashed line) and DSC (dashed-dotted line) curves of $ZnC_2O_4 \cdot 1.8H_2O-2FeC_2O_4 \cdot 2H_2O$ milled mixture heated at 5 K/min up to 500 °C under air flow.

value of $44.08 \pm 0.44\%$ well agrees with that expected for the formation of a mixture of ZnO and Fe₂O₃ (44.18%). The XRPD evidence confirms this point in that the reflexions present in the XRPD patterns of the residuals recovered from the TG runs are those characteristics of ZnO and Fe₂O₃ (no ZnFe₂O₄ has formed).

Fig. 3 shows a typical TG/DTG/DSC curve of a MM. It can be noted that the three mass loss steps are much less evident than in the case of the physical mixture. As concerns the first one, ending at ≈ 210 °C, the final mass of 77.75 $\pm 0.58\%$ is obtained. Such a value is lower than that expected for the complete dehydration of the oxalates. The following mass loss steps quantitatively correspond to the decomposition of the anhydrous oxalates to a mixture ZnO-Fe₂O₃. The final mass value is 42.86% that is lower than the value expected. The XRPD patterns of the residuals recovered after the TG runs actually show the reflexions of ZnFe₂O₄ only. Therefore, the final mass lower than expected allows to state that absorption of volatile impurities occurs during milling. The mass value expected for the release of these impurities during heating and for the mixture dehydration is 78.43%, that fairly agrees with the mean experimental mass value reached at $\approx 210 \degree C (77.75 \pm 0.58\%)$.

As concerns the DSC curve, after the first endothermic peak due to the dehydration of the mixture, two exothermic peaks are showing up. The first one has an enthalpy (mean of five independent measurements) of -437.5 ± 48.0 kJ. The mean mass loss under this peak is the sum of the mass loss due to reaction:

$$2\text{FeC}_2\text{O}_{4(s)} + (3/2)\text{O}_{2(g)} \to \text{Fe}_2\text{O}_{3(s)} + 4\text{CO}_{2(g)} \tag{1}$$

and to the decomposition of a fraction of Zn oxalate $(83.36 \pm 6.34 \text{ mol}\%)$ according to the following equation:

$$0.8336\text{ZnC}_2\text{O}_{4(s)} \rightarrow 0.8336\text{ZnO}_{(s)} + 0.8336\text{CO}_{(g)} + 0.8336\text{CO}_{2(g)}$$
(2)

From the literature [10] the enthalpies of reactions (1) and (2) are, respectively, $-278.15 \text{ kJ/mol FeC}_2O_4$ and $+136.73 \text{ kJ/mol ZnC}_2O_4$. Therefore, the value expected for the enthalpy of the first exothermic peak is: $(-278.15 \text{ kJ/mol FeC}_2O_4) \times 2 \text{ mol FeC}_2O_4 + (+136.73 \text{ kJ/mol ZnC}_2O_4) \times 0.8336 \text{ mol ZnC}_2O_4 =$



Fig. 4. XRPD patterns of $ZnC_2O_4 \cdot 1.8H_2O-2FeC_2O_4 \cdot 2H_2O$ mixtures heated at 5 K/min up to 500 °C under air flow: (a) milled mixture and (b) physical mixture. $ZnFe_2O_4$ (squares); ZnO (circles); Fe₂O₃ (lozenges).

-442.3 kJ that fairly agrees with the experimental value (-437.5 kJ).

As concerns the second exothermic peak the mean experimental enthalpy is -37.7 ± 2.5 kJ and the reaction under the peak is:

$$0.1664 ZnC_2O_{4(s)} \rightarrow 0.1664 ZnO_{(s)} + 0.1664 CO_{(g)} + 0.1664 CO_{2(g)}$$
(2')

So that the value expected for this peak is +22.8 kJ versus -37.7 kJ.

This means that an excess exothermic enthalpy of -60.5 kJ is present under the second exothermic peak that is related to the formation of ZnFe₂O₄.

The synthesis of ZnFe₂O₄ has been attempted by annealing (1 h) samples of MM at 500 °C: the mass loss at 500 °C (-57.59%) is in fair agreement with that obtained in TG analysis and the relevant XRPD patterns (Fig. 4a) of all the samples only show the reflexions of zinc ferrite though rather broad ones. By applying the equation of Scherrer to the XRPD line profile, the mean crystal size of 13.2 ± 1.6 nm has been calculated. The lattice constant of ZnFe₂O₄ obtained at 500 °C is 8.4355 ± 0.0056 Å, that is in fair agreement with that reported on the JCPDS file no. 022-1012 (8.4297 Å). The patterns of a sample of physical mixture subjected to the same thermal treatment (1 h at 500 °C) are shown in Fig. 4b: it can be seen that only the reflexions of both ZnO and Fe₂O₃ are present. An annealing at 1000 °C is needed to complete the ZnFe₂O₄ formation when starting from a physical mixture. The nanometric size of the MM sample calculated from XRD line broadening is confirmed by observing the SEM micrograph shown in Fig. 5.

3.1.2. $ZnC_2O_4 \cdot 1.8H_2O-Fe_2(C_2O_4)_3 \cdot 6H_2O$ mixtures

Fig. 6 shows a typical TG/DTG curve of a sample of PM: the first stage is a double one and the mean mass value at the first relative DTG minimum (≈ 200 °C) is 66.88 ± 1.51%.

As a matter of fact it is known from the literature [11,12] that the reduction of iron(III) oxalate to iron(II) oxalate occurs during



Fig. 5. SEM micrographs of $ZnC_2O_4 \cdot 1.8H_2O-2FeC_2O_4 \cdot 2H_2O$ milled mixture annealed 1 h at 500 °C in air.

the course of dehydration according to the following reaction:

$$Fe_2(C_2O_4)_3 \cdot 6H_2O_{(s)} \rightarrow 2FeC_2O_{4(s)} + 2CO_{2(g)} + 6H_2O_{(g)}$$
 (3)

The mass value of 65.87% is to be expected if reaction (3) and zinc oxalate dehydration occur. The experimental mass value higher than expected can be justified if only a partial reduction of Fe(III) to Fe(II) would occur and, in this sense, the moles of iron(III) oxalate not reduced before $\approx 200 \,^{\circ}$ C are 0.08.

The following stages show a total mean mass loss of $-12.96 \pm 0.55\%$. The separation between the two stages is rather poor. However, the XRPD patterns of the residuals show that a mixture ZnO–Fe₂O₃ has actually formed.

Fig. 7 shows a typical TG/DTG/DSC curve of a sample of MM. Also in the case of this milled mixture the mass loss steps are much less evident that in the physical mixture. No mass value corresponding to that expected if reaction (3) would occur can be individuated. Moreover the mass loss is over at a lower temperature than with the PM. The XRPD patterns of the residuals show only the peaks of $ZnFe_2O_4$.

As concerns the DSC traces, two exothermic peaks are present. The first one has an enthalpy (mean of six inde-



Fig. 6. TG (solid line) and DTG (dashed line) curves of ZnC_2O_4 ·1.8H₂O-Fe₂(C₂O₄)₃·6H₂O physical mixture heated at 5 K/min up to 500 °C under air flow.



Fig. 7. TG (solid line), DTG (dashed line) and DSC (dashed-dotted line) curves of $ZnC_2O_4 \cdot 1.8H_2O$ -Fe₂(C_2O_4)₃·6H₂O milled mixture heated at 5 K/min up to 500 °C under air flow.

pendent measurements) of -486.1 ± 44.2 kJ. The mass loss under the peak is a little lower than with the Fe(II)-based mixture. By hypothesizing that the reduction of Fe(III) oxalate to Fe(II) oxalate takes place, the enthalpy balance of the first exothermic peak can be set as follows: (-278.15 kJ/mol $\text{FeC}_2\text{O}_4) \times 2 \text{ mol} \text{FeC}_2\text{O}_4 + (+136.73 \text{ kJ/mol} \text{ZnC}_2\text{O}_4) \times 0.7989$ mol $\text{ZnC}_2\text{O}_4 + Y = -486.1$ kJ, with Y = -39.0 kJ.

The fact that in the case of the present reacting system, an excess of exothermic enthalpy is present also under the first peak means that some other process (very likely the Fe(III) oxalate reduction) is going on.

As concerns the second exothermic peak the mean experimental enthalpy is -39.0 ± 5.8 kJ and the reaction under the peak is:

$$0.2011 \text{ZnC}_2\text{O}_{4(s)} \rightarrow 0.2011 \text{ZnO}_{(s)} + 0.2011 \text{CO}_{(g)} + 0.2011 \text{CO}_{2(g)}$$
(2")

So that the enthalpic balance under this peak is: -39.0 kJ = $(0.2011 \text{ mol } ZnC_2O_4) \times (136.73 \text{ kJ/mol } ZnC_2O_4) + Z$, with Z = -66.5 kJ.

It can be noted that the excess of exothermic enthalpy under the second peak is nearly the same as that obtained (-60.5 kJ)with the Fe(II)-based mixture. Therefore, it is confirmed that an excess of exothermic enthalpy (-60.5 kJ) is related to the formation of ZnFe₂O₄.

ZnFe₂O₄ has been obtained from samples of milled mixture annealed in a furnace for 1 h at 500 °C (air). The relevant XRPD patterns of the sample only show the reflexions of zinc ferrite though rather broad ones (Fig. 8a). By applying the equation of Scherrer to the XRPD line profile, the mean crystal size of 14.2 ± 1.1 nm is obtained. The lattice constant of ZnFe₂O₄ obtained at 500 °C has been determined. The value of 8.4297 ± 0.002 Å is in fair agreement with that of ZnFe₂O₄ obtained starting from Fe(II) oxalate. The patterns of a sample of physical mixture subjected to the same thermal treatment (1 h at 500 °C) are shown in Fig. 8b: it can be seen that only the reflexions of both ZnO and Fe₂O₃ are present. An annealing at 1000 °C is needed to complete the ZnFe₂O₄ formation when starting from a physical mixture. The nanometric size of the MM



Fig. 8. XRPD patterns of ZnC_2O_4 ·1.8H₂O-Fe₂(C₂O₄)₃·6H₂O mixtures heated at 5 K/min up to 500 °C under air flow: (a) milled mixture and (b) physical mixture. ZnFe₂O₄ (squares); ZnO (circles); Fe₂O₃ (lozenges).

sample calculated from XRD line broadening is confirmed by observing the SEM micrograph shown in Fig. 9.

4. Magnetic properties

The uppermost panel of Fig. 10 shows the magnetization as a function of temperature for powders of $ZnFe_2O_4$ obtained from:

- (a) Mixture $ZnC_2O_4 \cdot 1.8H_2O 2FeC_2O_4 \cdot 2H_2O$ milled and annealed 1 h at 500 °C (sample 1).
- (b) Mixture ZnC₂O₄·1.8H₂O−Fe₂(C₂O₄)₃·6H₂O milled and annealed 1 h at 500 °C (sample 2).
- (c) Mixture $ZnO-Fe_2O_3$ annealed 36 h at 1000 °C (sample 3).

It can be seen that all samples are paramagnetic at high temperature and anti-ferromagnetic below a temperature (T_N). For sample 3, the transition is broader and the transition temperature T_N is larger (nearly 60 K) that for samples 1 and 2 (nearly 35 K). It is well known that the normal ZnFe₂O₄ spinel has $T_N \approx 10$ K and it is also known that the partial inversion of spinel structure results in an increased T_N [13]. Hence, our data seem to indicate that sample 3 has a mixed spinel structure, whereas in



Fig. 9. SEM micrographs of $ZnC_2O_4\cdot 1.8H_2O\text{--}Fe_2(C_2O_4)_3\cdot 6H_2O$ milled mixture annealed 1 h at 500 $^\circ\text{C}$ in air.



Fig. 10. Upper panel: magnetization as a function of temperature in an applied field of 100 Oe for sample 1 (squares), sample 2 (circles) and sample 3 (triangles). The open symbols are used for the zero field cooled curves, while the filled symbols are used for the field cooled curves. Lower panel: hysteresis loops of sample 1 (squares), sample 2 (circles) and sample 3 (triangles) measured at temperature 5 K. In the inset, a zoom of the low field region is presented, showing the enhanced coercive field of samples 1 and 2.

samples 1 and 2 the presence of the inverted spinel structure is less important.

The magnetization peak at the transition temperature for the three samples (at 100 Oe) is 2.9 emu/g (1), 2.5 emu/g (2) and 0.66 emu/g (3). These values are consistent with those reported for a nanocrystalline $ZnFe_2O_4$ powder [6].

Magnetic hysteresis loops have also been measured at different temperatures (5, 35, 100, 200 and 300 K) in magnetic fields up to 5 T. The lower panel of Fig. 10 shows the measurements at 5 K in the three samples. It can be seen that saturation is not yet attained even at 5 T, due to the presence of a linear and reversible contribution, which becomes increasingly preponderant with increasing temperature. Such behaviour indicates the presence of a paramagnetic phase, as it has already pointed out by other authors [6]. In the inset, a zoom of the low field region is shown, where it can be seen that at 5 K the coercive field is as large as 630 Oe for samples 1 and 2 and 320 Oe in the case of sample 3. The coercive field at 35 K, though small, has a finite value only in the case of samples (1 and 2) prepared starting from the milled mixtures. At higher temperatures, the coercive fields of all the samples are vanishingly small. Lopez et al. [14] synthesized nanocrystalline $ZnFe_2O_4$ powder with a remnant magnetization of 0.066 emu/g and a coercive field of 13 Oe; in comparison, the values of coercive fields found in our samples 1 and 2 are quite high. It seems that the synthetic procedure (milling + low temperature annealing) yields significant enhancement of the "pinning" of the magnetic domains, as a direct consequence of the sample microstructure.

5. Conclusions

- In order to synthesize $ZnFe_2O_4$, the solid state reactions in the systems $ZnC_2O_4 \cdot 2H_2O 2FeC_2O_4 \cdot 2H_2O$ and $ZnC_2O_4 \cdot 2H_2O Fe_2(C_2O_4)_3 \cdot 6H_2O$ have been studied. Independently on the iron precursor selection (Fe²⁺ or Fe³⁺). It has been shown that the mechanical activation of the starting systems results in the formation of $ZnFe_2O_4$ within 500 °C while only a mixture $ZnO Fe_2O_3$ is produced when starting from the unmilled mixtures. The enthalpy of $ZnFe_2O_4$ formation starting from the constituent oxides has been estimated.
- One hour-annealing of the activated mixtures at 500 °C in air yields nanocrystalline ZnFe₂O₄ while prolonged annealing at 1000 °C is needed to obtain microcrystalline ZnFe₂O₄ when starting from the corresponding non-activated systems.
- The proposed synthetic procedure (milling + low temperature annealing) yields significant enhancement of the "pinning" of the magnetic domains, as a direct consequence of the sample microstructure.

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